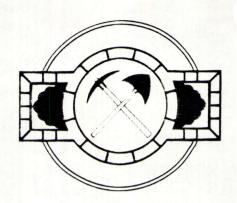
WESTERN INTERNATIONAL CORPORATION 1399 South 700 East, Suite 16 Salt Lake City, Utah 84105 Telephone: (801) 487-7522 June 4, 1981 Mr. Lee Spencer Division of Oil, Gas and Mining 1588 West North Temple Salt Lake City, UT 84116 Dear Lee: Park City Planning Commission had asked us for more detailed information on our project which we put together for them. It includes such things as equipment specs, more detailed plan of operations, etc. I have enclosed a copy for your department as I promised you I would at the meeting last night. We really appreciate the way you have been working with us and your cooperative attitude. Thanks a million. Best regards, LaVar Engle Area Director LE/sm Enclosures

WESTERN INTERNATIONAL CORPORATION

OPERATIONAL IMPACT STUDY



P O BOX 1480 PARK CITY, UTAH 84060 PHONE (801) 649-9321

May 14, 1981

Mr. LaVar Engle Mr. Dennis Engle 1399 South 700 East Suite 16 Salt Lake City, Utah 84105

Dear Sirs:

This letter is to confirm our meeting of this morning and give you in better form the notes I copied for you.

I must stress the need to quantify and put in written form the possible impacts of your operation and how you propose to minimize those impacts. As you are aware residents in the area are very concerned about the possible impacts on their property and lifestyle. The following items are ones which I see at this time as needing detailed clarification.

1. Machinery specification - including motor sizes and types, decibel levels, and emmissions.

2. Grading plan - including temporary and permanent stream treatment, dust control techniques and revegetation plans.

3. Flood control Plan.

4. Water rights and availability and estimated useage.

5. Operations plan including number of employees, hours of operation, traffic volume, method of transporting material on and off site, and structures to be constructed, i.e. restrooms, equipment storage and servicing, fencing or buffering desireable.

6. Bonding procedure - BLM procedure to assure revegetation.

7. Park dedication.

Receipt of BLM Environmental Study and your survey, both now in progress will provide us with additional information. It is imperative that we receive all of the above data at least one week before County Planning Commission so that we may fairly evaluate it and prepare comments. I think you will find that incomplete information will only slow the review progress.

MACHINERY SPECIFICATIONS

MACHINERY SPECIFICATIONS

Enclosed are the specifications for the equipment which will be used at the Silver Maple Mine site as provided to us by the manufacturers.

The noise levels of the Caterpillar Equipment will be impacted by the distance from the homes of Prospector Square at which it will be operated and by the buffer row of trees that will be established. Each year the noise impact becomes less because the distance of separation becomes greater and the trees grow larger.

The noise levels of the other equipment will be insignificant because of the distance involved versus the size and type of motors.



Brother's Mining And Manufacturing, Inc. P.O. Box 422 Molalla, OR 97038 503-829-5090 503-829-8789

503-829-5090 503-829-8789

May 18, 1981

Engle Development Co 1339 8, 700 E Suite 16 Salt fake City, litab 84105

dear dennie,

as per our conversation May 15, 1981. Sam sending what information I have relevent to the noise level of our mening iquipment The motors are a 3 phase 5 horsepower 226-440 voet (or we can got single phase 220) Baidor electric motors which would make less noise than an electric fan. The other possible source of noise would be the rock in the rotating barrel. The main factor which will affect how much noise will be produced would be the size of the material. being processed through the concentration. If you process I inch minus or smaller material as 7 discussed with you earlier, the noise tevel would be quite low. The fact that rock works in water in the concentrator serves to keep the noise level low.

I can really appreciate the concern for ix-Cessive norse in an area like Park City and 9 cans assure you that our equipment will, produce a noise level well within reasonable standards forthat area. In those places where we have usedour equipment we find that the loader is actually

sairsier than the concentrator.

I find the brothere you wanted did not contain ultat you wanted but if you wish we will mail you one later. yours truly, Len Harri

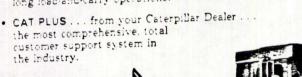


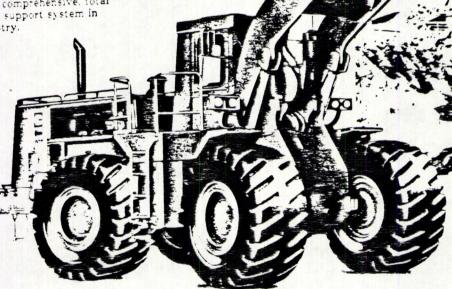
CATERPILLAR

* INSIDE CAR NOWE LEVEL = 94 Decibles

Summary of features

- Rated foad . . . 9600 kg -21,200 lb.).
- Cat 3408 diese! Engine . . . with 18.0 liters (1,099 cu in.) displacement.
- · High breakout force . . . excellent loadability.
- Single lever power shift... fast, easy speed and direction changes
 four speeds forward, four reverse.
- Variable capacity torque converter... lets operator apportion power between hydraulics and drive train.
- Four wheel oil disc brakes . . . adjustment-free and completely sealed from dirt and grit.
- Sealed loader linkage . . . extends lube intervals, reduces maintenance time.
- Servicing ease... with centralized servicing center, two-section hood for engine and torque converter removal, demountable rims.
- Optional Beadless Tire arrangement for loading shot rock and long load-and-carry operations.





Sound-suppressed cab and ROPS shown are standard.



Caterpillar Engine

Kilowatts @ 2200 RPM 280 Horsepower 200 RPM 280

(Kilowatts (kW) is the International System of Units equivalent of horsepower.)

The net power at the flywheel of the vehicle engine operating under SAE standard ambient temperature and barometric conditions, 29° C (85° F) and 995 m.bar (29° 38° Hg), using 35 API gravitions, 29° C (60° F), and after deductions for fan, air fuel oil at 15 6° C (60° F), and after deductions for fan, air cleaner, water pump, lubricating oil pump, fuel pump alternator and muffler. No derating is required up to 2300 m (7,500 ft.) altitude.

Caterpillar four-stroke-cycle. 3408 diesel Engine. 65° V-8 with 137 mm (5.4") bore, 152 mm (6.0") stroke and 18.0 liters (1,099 cu in.) displacement.

Turbocharged, direct injection fuel system. Integral inlet manifold porting with two intake and two exhaust valves per cylinder. Valves

are actuated by a pushrod mechanism. Single camshaft is mounted into "V" of engine. Variable timing fuel system. Adjustment-free fuel pumps, non-clogging injection valves.

24-volt direct electric starting system with ether starting aid standard (Ether canister not included.)



transmission

Cat planetary type. Full power shift in four forward and four reverse speeds.

Single lever on left side of steering column controls both speed and direction. Rotate the handle for four speed ranges in forward and reverse. Move the lever forward or backward for directional change. Transmission lever is locked in neutral by moving steering column to forward-most position.

Variable capacity torque converter lets operator match rimpull to specific application.

Wheel Loader

transmission (continued)

Maximum speeds, forward and reverse, with 65:35:33, 24 PR (L-4) tires:

	1st	2nd	3rd	4th
Forward, km h	6.4	11.5	20.4	36.2
MPH	4.0	7.2	12.7	22.5
Reverse, km h	7.4	13.2	23.3	41.4
MPH	4.6	8.2	14.5	25.7

Maximum speeds, forward and reverse, with Beadless Tires:

	1st	2nd	3rd	4th
Forward, km h	6.1	10.9	19.5	34.6
MPH	3.8	6.8	12.1	21.5
Reverse, km h	7.1	12.6	22.2	39.4
MPH	4.4	7.8	13.8	24.5



Front axle fixed, rear axle oscillates ± 13°. One rear wheel can drop or rise a total of 560 mm (22 0") with all wheels remaining on ground for maximum traction. Free-floating axle shafts can be removed independently of wheels and planetaries. Conventional differentials

final drives

All-wheel drive with planetary reduction in each wheel. Torque is developed at the wheel, putting less stress on axle shafts. Planetary units can be removed independently of wheels and brakes.

brakes

System meets OSHA regulations.)

Service - Four wheel, full-hydraulic, fully enclosed oil-disc type. Self-adjusting Fade-resistant, with smooth modulation Two brake pedals, right pedal brakes only, left pedal brakes while neutralizing transmission.

Parking - Spring-applied, dry disc parking brake acts on main drive line Operator applies manually.

Emergency - Uses parking brake on main drive line If hydraulic pressure drops below 69 bar 1000 psi when transmission is engaged. an audible alarm sounds, then brake automatically applies to bring machine to a controlled stop Operator may also apply manually A red light warns when pressure to parking brake drops

tires

beless, low aspect ratio, bias belted, loader-dozer de-65 35-33. 24 PR (L-4)

65 35-33, 24 PR (L-5)

In certain applications such as load-and-carry work, the productive capabilities of the loader may exceed the Ton-MPH capabilities of standard or optional tires. This restriction could be the limiting factor in the use of the vehicle

Caterpillar recommends that the user consult his tire supplier to evaluate all conditions affecting tire life and costs in order to make proper tire selection.

Beadless Tires

Caterpillar steel shoe Beadless Tires are an optional arangement with one-piece complete oval air chamber, helically wound with steel cable, and a separate, replaceable, cablereinforced rubber mounting belt. Steel shoes bolt directly to anchor places moided into mounting belt. Rim is two-piece, bolted together. No Ton-MPH limitation

Number of shoes Size of shoes

178×530 mm (7.0 × 32.6")

steering

Center point frame articulation. Rear and front wheels track. Full hydraulic power with flow amplified system.

Flow to steering cylinders is controlled by a steering wheel-operated metering pump. Full-flow filtering.

Minimum turning radius (over tire) (§) 7870 mm (25.10") Steering angle (each direction)

Hydraulic system - Two 127 mm (5.0") bore, double-acting cylinders powered by the large section of a double-section gear pump.

Output @ 2200 RPM with 382 liters min (101 gpm) 69 bar (1000 psi) 172 bar (2500 psi) Relief valve setting



bucket controls

Lift circuit - Positions: Raise, hold, lower and float. Automatic kickout adjustable from horizontal to full lift height.

Tilt circuit - Positions. Roll back, hold and dump. Automatic bucket positioner adjustable to desired loading angle

No visual spotting required.



lift arm pins

Sealed - 100 working hour lube intervals except lower bucket pins, which need lubrication only every 2,000 work-



loader hydraulic system

Closed with pressure control - 1.4 bar (20 psi) vacuum relief. Pilot-operated controls.

Single gear pump for implement system. Output @ 2200 RPM and 69 bar (1000 psi), with SAE No 10 oil @ 66° C (150° F)

520 liters min (137 gpm) 207 bar (3000 psi) Relief valve setting

Small section of double-section gear pump for pilot and brake systems:

Output @ 2200 RPM and 100 liters min (26 4 gpm) 69 bar (1000 psi) 152 bar (2200 psi) Relief valve setting

Cylinders (double acting): 216×1140 mm. (5.5"×45.0") 196×720 mm. (7.75"×28.5") Lift - bore and stroke Tilt - bore and stroke

Hydraulic cycle time rated load in bucket, in seconds \$10

		Lower (empty.	
Raise	Dump	float down)	Total
9.4	3 0	4 .5	16.9



service refill capacities

		11.6 6-11
	Liters	U S Gallons
Cooling system	106	25
Crankcase	41.6	11
Transmission	102	27
Differential and final drives:		
Front	204	54
Rear	204	54
Hydraulic tank	235	62
Fuel tank	620	165
I UEL . a.i.h		



Cab plus ROPS is standard)

ROPS Rollover Protective Structure offered by Caterpillar for this machine meets ROPS criteria. SAE J394. SAE J1040a and ISO 3471. It also meets FOPS Falling Object Protective Structure) criteria SAE J231 and 180 3449.

Operating Specifications

the state of the s	-		V-Edge	A service of the service of	-	Streight Edge			
		1	Rock	Rock		Rock	Ligi		
Bucket Type Rated load/6)	1 July	Rock	With Teeth	Modulok	Rock	With Teeth	Mate		
Rated load(§)	kg	9600 21,200	9600 21,200	9600 21,200	9600	9600 21,200	960 21,2		
Capacity, heaped	m ³	5.35	5.35	5.35	5.35	5.35	6.1:		
	yd^3	7.00	7.00	7.00	7.00	7.00	8.01		
Capacity, struck(§)	m ³	4.51	4.51	4.43	4.59	4.59	5.1:		
	yd3	5.90	5.90	5.80	6.00	6.00	6.71		
Width(§)	mm	3630	3630	3650	3630	3630	363		
	ft	11'11"	11'11"	11'11.5"	11'11"	11 11"	11'1		
Dump clearance @ full lift and 45° discharge(§)	mm	3450	3175	3265	3710	3480	353		
[12] [2] [2] [2] [2] [2] [2] [2] [2] [2] [ft	11 4"	10'5"	10'9"	12.2	11'5"	11'7		
Reach @ full lift and 45° discharge(§)	mm	1930	2110	2065	1650	1880	180		
	ft	6'3"	6 11"	6'9"	5'5"	6'2"	5'11		
Reach @ 45° discharge angle,		1 00	0	0.5	33	02	311		
2130 mm (7'0") clearance(§)	mm	2440	2740	2730	2440	2620	2541		
	ft	8'0"	9'0"	8'11"	8.0.	8'7"	84'		
Reach with lift arm horizontal and bucket level	mm	3480	3810	3725	3100	3430	3330		
	ft	11'5"	12'6"	12'3"	10'2"	11.3"	10'11		
Digging depth(§)	mm	69	122	116	69	75	96		
	in	2.70"	4.82"	4.60"	2.70"	2.95"	3.80		
							0.00		
Overall length(§)	m	10.39	10.72	10.62	10 01	10.31	10.2		
[12] [14] [14] [14] [15] [15] [15] [15] [15] [15] [15] [15	ft	34 1"	35 2"	34 10"	32'10"	33 10"	33'6		
Overall height(§)	m	6.93	6.93	6.93	6.50	6.50	6.76		
	ft	22.9"	22'9"	22'9"	21'3"	21 4"	22 2'		
Loader clearance circle (bucket in carry position)(§)	m	17.02	17.22	17.20	17.07	17.17	17.17		
	ft	55'10"	56'6"	56'6"	56'0"	56 4"	56'4'		
Static tipping load,**									
Straight(§)	kg	22 450	22 090	21 480	23 160	22 980	22 33		
	lb	49,500	45,700	47,355	51,060	50.680	49.24		
Full 35° turn(§)	kg	20 290	20 000	19 190	21 010	20 790	20.03		
	lb	44,740	44,100	42,310	46,320	45,840	44.17		
Breakout force*(§)	kN	362	359	380	466	464	397		
	kg	3€ 650	36 380	38 500	47 220	47 040	40 190		
	lb	80.800	80,200	84.880	104.100	103.700			
		00,000	80,200	64,000	104,100	103,700	88.660		
Operating weight**	kg	38 930	39 200	39 620	38 650	38 810	38 920		
	1b	85,830	86,420	87.345	85,200	85.560	85.800		
With Beadless Tires:						00,000	30,300		
Static tipping load,	4 18								
Straight(§)	kg	24 720	24 440	23 820	25 530	25 310	24 900		
	lb	54,500	53,900	52.514	5€.300	55.800	54.900		
Full 35° turn(§)	kg	22 220	21 930	21 120	22 990	22 770	22 400		
	lb	49,000	48,350	46,560	50.700	50.200	49.400		
Breakout force*(§)	kN	360	7.70	200	.00				
sicular force (8)	7.5		357	380	463	461	396		
	kg	36 440 80,340	36 170 79,740	38 500	46 940	46 770	40 110		
	10	0,540	75, 40	84,880	103,480	103,100	88,420		
Operating weight	kg	42 480	42 750	43 170	42 200	42 360	42 470		
	lb	93,650	94,240	95,165	93.020	93.380	93.620		

Measured 102 mm (4.0) betind tip of curring edge with bucker nige pin as proving that it is a conditioner 65.35.24 PP Li4 tires, full fue tank and operating weight shown include sound suppressed tabland PDPS with a roond tipner 65.35.32.4 PP Li4 tires, full fue tank and operating weight are affected by fire ballast and attachments. For additional state of ping table past of purposed for the past and state of ping to additional state of the past and state of ping table past and state of the past and st

	Operating Weight		Static Tipping Load	
	Kg	Lb	Kg	Lb
Remove ROPS canopy and cab	-1170	-2.570	- 910	-2.010
Remove cab only	- 270	- 600	- 190	- 410
Remove ROPS canopy only	- 890	-1.970	- 730	-1.600
Add counterweight	+1630	+3,600	+3090	+6.520
65 35-33, 24 PR (L-4) tires with 75% CaCl ₂	+2630	+5,500	+3150	+7.020
65 35-33, 24 PR (L-5) tires	+ 585	+1.290	+ 360	+ 500
65 35-33, 24 PR (L-5) tires with 75% CaCl ₂	+2900	+6.400	-3220	+7.100

Specifications and ratings conform to all applicable standards recommended by the Society of Automotive Engineers SAE Standard J732c (1969) and SAE Standard J742b (1969) govern loader ratings denoted in the text by §).

hydraulic controls

Complete system consists of pump, tank, filter, valves, lines, linkage and control levers. Hydraulic pilot controls take most of the effort out of operating the ripper and dozer tilt levers. The six optional hydraulic systems, all with external valves, include:

One valve, for SA Bulldozer	950 lb. (430 kg)
Two valves, for 8S or 8U Bulldozer and tilt	1,165 lb. (528 kg)
Two valves, for 8A Bulldozer and ripper with manual adjustment	1,070 lb. (485 kg)
Three valves, for 8A Bulldozer and ripper with hydraulic adjustment	1,175 lb. (533 kg)

Three valves, for 8S or 8U Bulldozer, tilt 1.280 lb. (580 kg) and ripper with manual adjustment

Four valves, for 85 or 80 Bulldozer, tilt and ripper with hydraulic adjustment

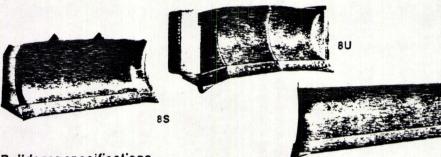
Pump: 78 gpm (295 litres/min) Output @ 1000 psi (69 bar) 22 gpm (83 litres/min) Tilt cylinder flow 1885 RPM @ rated engine speed

Relief valve settings: 2400 psi 166 bar) Bulldozer 2400 psi (166 bar) 2500 psi (172 bar) Ripper Tilt cylinder Geared from auxiliary drive Drive Contro! valve positions:

Raise, hold, lower, float Bulldezer Raise, hold, lower Ripper Tilt right, hold, tilt left Tilt cylinder Reservoir: Fender Mounting

185 gallons (70 litres)

1.300 lb. (590 kg)



Rugged D8K bulldozers have durable DH-2 cutting edges and end bits. Push arm braces connect to a sliding center ball that absorbs side stress on push arms and blade. A single lever controls all blade movement, including tilt.

Bulidozer specifications

Blade	Overall Width (tractor with bulldozer)	Height	Diggin g Depth	Ground Clearance	Maximum Tilt	Weight**	Total Operating Weight *** (tractor with bulldozer)
8 S	13'3" *	5'0"	20" (510 mm)	4'7" (1400 mm)	40" (1020 mm)	12.050 lb. (5450 kg)	70,500 lb. (31 979 kg)
8U	(4040 mm) 13'11" * (4240 mm)	(1520 mm) 5'0" (1520 mm)	20" (510 mm)	4'7" (1400 mm)	41.7" (1060 mm)	13,310 lb. (6040 kg)	71,700 lb. 32 523 kg)
8.A, straight	15'6" *† (4720 mm)	3'8" (1120 mm)	24.2" 610 mm)	4'4" (1320 mm)	13" (330 mm)	11,590 lb. (5260 kg)	69,800 lb. (31 661 kg)
Angled 25°	14'0" (4270 mm)	3'8" (1120 mm)	3 1" (790 m m)	5'2" (1570 mm)	13" (330 mm)		

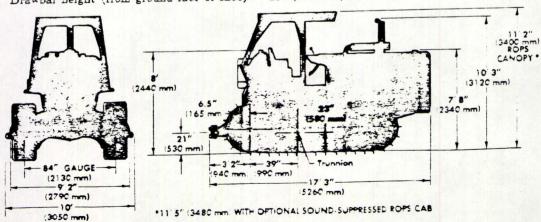
Tank capacity

-Width with C frame only is 11.5 (3480 mm).

**Does not include hydraulic controls, but 8S and 8U include blade tilt by inder.

dimensions (approximate)

Ground clearance, from ground 17.1" (434 mm) 21" (530 mm) face of shoe (per SAE J894) Drawbar height (from ground face of shoe)

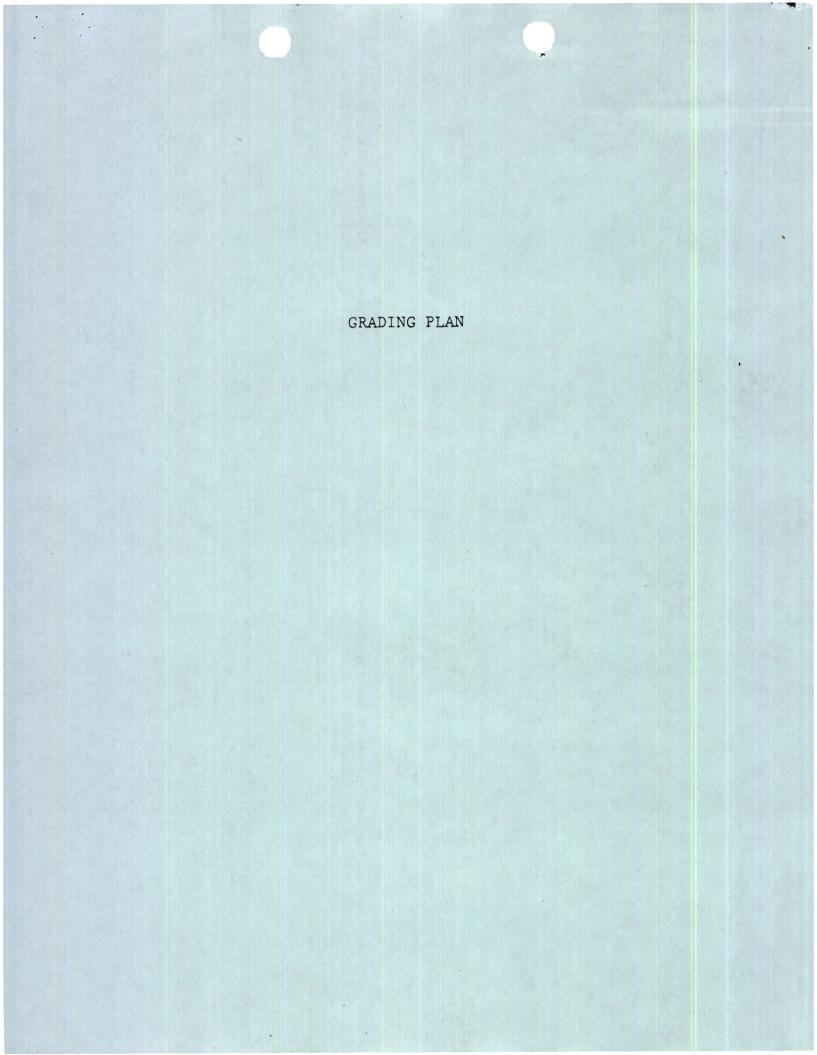


WITH FO			
17 3			
SMELL	CHANK		(Cmm)

SINGLE SHANK RIPPER	6 7	(2010 mm)
MULTSHANK RIPPER	5 0	(1520 mm)
5 DOZER	4 4	(1320 mm)
U - DOZER	5 5	(1650 mm)
A - DOZER	4 5	(1350 mm)
A DOZER	7 5	(2260 mm)
C. FRAME ONLY	2 8	(810 mm)

^{*}Width over hot supped end bits. Width over standard forged end bits is 4 (102 mm) 'ess.

^{***}Includes hydraulic controls, blade tilt cylinder (8S and 8U), lubricants, coclant, full fuel tank, RCPS canopy and operator



PROJECTED MINING OPERATIONS

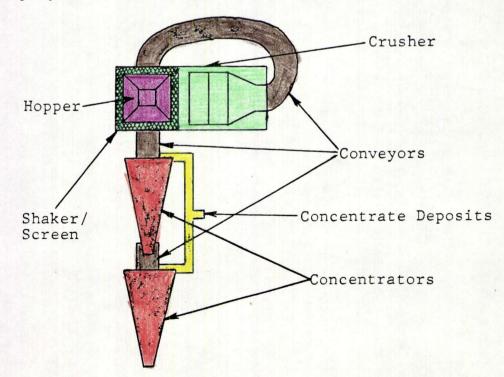
GRADING PLAN:

The enclosed drawings represent the year-to-year proposed mining process for the Silver Maple Mine, inclusive of Maple #1, Maple #2, Maple #3, and Maple #4 mining claims. This report reflects the projected mining activities on Maple #1 and Maple #2 mining claims, and all calculations are based upon a uniform tailings depth of ten (10) feet. A significant variance in the depth of the tailings would alter the time schedule of the proposed mining sequence.

On-going regrading or recontouring of the area will be accomplished as stipulated in the Bureau of Land Management Environmental Impact Study, and the contour and ground level will be restored in a manner suitable for a park site and such determinations shall be correlated with the Park City Planning Commission.

The sequence beginning at the west end of both Maple #1 and Maple #2 will include the movement of the entire tailings in the proposed excavation area through a small roll crusher and two concentrators. As much material to maintain uninterrupted operations will be piled near the concentrator sites, since the dozer will be operating only as required, perhaps as little time as one to two weeks during the mining seasons. Each year the excavated area will be restored, compacted and regraded to the specifications compatable to a future park site.

The following drawing illustrates the basic process to be employed:



As a result of recent spectographic analysis of the tailings, consideration is being given to the possibility of removing all tailings from the mine site and to transport them to a potential processing millsite, to be located on Maple #3. The eventuality of this consideration will be determined through extractive metallurgy consultation and research to determine the feasibility of extracting precious minerals other than gold and silver. Such determination will be made following the 1981 mining season and will be conditional based upon the approval of regulatory bodies. In the event the above consideration is realized, the concentrating process would be removed from Maple #1 and Maple #2 and the excavated area would be processed from west to east and thereafter refilled and leveled prior to the completion of the then current mining season.

STREAM TREATMENT:

As evidenced on the mine site, Silver Creek has been subjected to a prior stream diversion and the proposed temporary rechanneling provides that the stream be retrenched on the north-westerly extremities of the property and to run parallel to the existing canal.

A headgate will be strategically placed at two locations on the stream to provide a means to replenish water stored in two separate settling ponds. Such diversion methods will provide that there will be no comingling of the water from Silver Creek with that from the settling ponds.

The stream channel will be dug to a minimum depth and width of three feet (3') and will exceed these minimums in areas where required to maintain a natural gravity flow. A thirty six inch (36") galvanized pipe will be placed in the diversion channel and canal under the access road to the property.

This diversion will serve only as a temporary placement and further re-channeling will be accomplished consistant with the requirements of the Park City Planning Commission under the consideration of a park site.

DUST CONTROL:

At this time dust is not considered to be a major concern because the nature of the crushing and washing methods involve a "wet process". Also due to the physical configuration of the tailings, dust is inherently reduced, especially considering that a large portion of the tailings are currently under water and that the water table is very shallow and that a degree of water saturation is evidenced on entire tailings deposit.

From an operational stand-point dust should be minimized. The tailings when processed will most generally be damp and would result in very little dust emission when crushed. Thereafter the product is washed and sized through spiral concentrators using approximately four hundred (400) gallons of recirculated water per minute. From all considerations, dust should be greatly controlled and the impact should be minimal especially considering that the extraction process will be situated in excess of four hundred (400) yards removed.

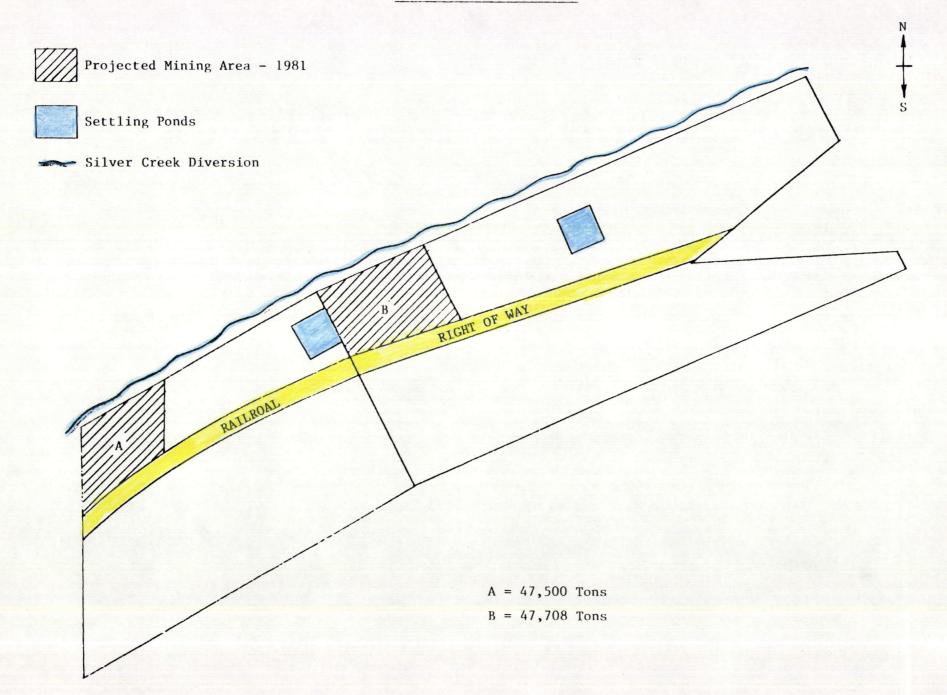
In the event that dust does become a problem, an acceptable method of screening will be employed to control the difficulty.

REVEGETATION PLAN:

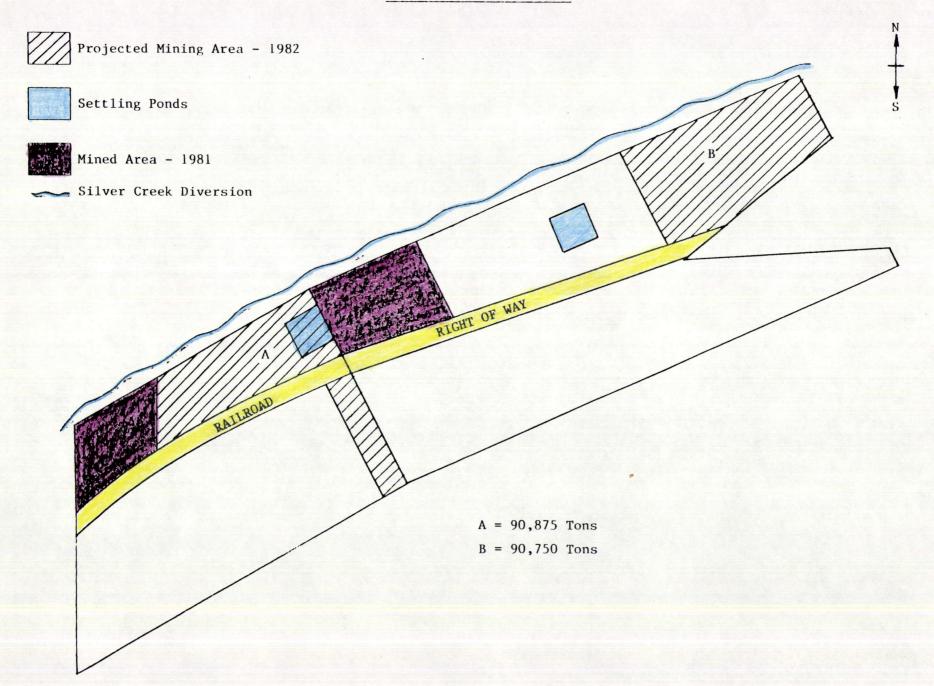
Revegetation will be completed each year of operation and will include leveling and recontouring. Reclamation will be complete in compliance to the recommendations of the Bureau of Land Management provided in their Environmental Impact Study.

There is a consideration that the mining site may be donated to Park City for the purpose of constructing a park site, providing that certain conditions can be mutually agreed upon between Park City and Western International Corporation. Restoration thereby would be completed in the form of a public park and would be developed with the cooperation of the Park City Planning Commission.

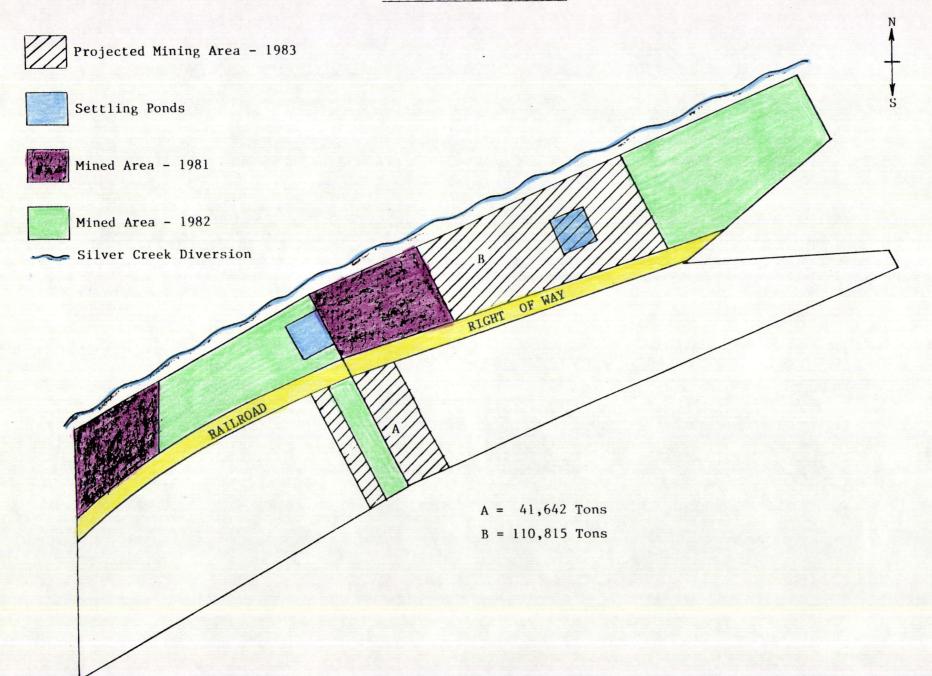
1981 MINING PROJECTIONS



1982 MINING PROJECTIONS



1983 MINING PROJECTIONS



FLOOD CONTROL PLAN

FLOOD CONTROL

The current stream bed of Silver Creek is poorly defined.

It has been rechanneled several times, is shallow, and is infested with small beaver dams which have created silt filled ponds. The proposed diversion of Silver Creek will give it a well defined channel on the north side of Maple 1 and 2 claims.

The existing channel will serve as a natural runoff site for any waters rushing over disturbed areas. The two ponds (see the grading plans) have a capacity exceeding 100,000 cubic feet each. They will be excavated ponds, rather than the typical dam or dike, therefore eliminating any possibility of breaking through a dam and creating worse flooding. There will be a small dike built and it will have overflow culverts built in.

The culverts under the proposed access road on both the irrigation canal and diversion channel will be 36" galvanized pipe which will be sufficient to handle any 24 hour storm runoff anticipated.

WATER USEAGE

WATER RIGHTS AND USAGE

The water rights for the Silver Maple Mine operations are being acquired from Stanley Pace through the purchase of land. We will own 3% of the total flow of Silver Creek and Doherty Springs. Per the BLM Environmental Impact study, the current flow of Silver Creek is .9 C.F.S. and Doherty Springs is 2 C.F.S. and 3% of that flow equates to 53,369 gallons per day.

Each concentrator on the mine site will use 200 gallons per minute of water. Strict measures, i.e. lined return ditches, water catching facilities under the equipment, etc., will be taken to save and conserve water. The basic water loss will be from evaporation since all water is recycled. Maximum water loss will be less than 10%. Our water supply is 53,369 gallons per day with maximum irreplaceable usage at 40 gallons per minute or 28,800 gallons per 12 hour day. That means we have enough water to double our operations.

OPERATIONS PLAN

OPERATIONAL PLAN

EMPLOYEES:

It is anticipated there will be between four to seven employees on site during the mining season. The variation will be determined by the number of concentrators stationed on site and by the number of front-end loaders. The anticipated maximum number of employees is outlined as follows:

Foreman

- (2) Truck Driver/Laborers
- (2) Front-end Loader Operators
- (2) Crusher/Concentrator Operators

HOURS OF OPERATION:

It is anticipated that the work day will commence at 7:00 a.m. and physical operations of the equipment will be for approximately eleven (11) hours.

TRAFFIC VOLUME:

A transport vehicle will be used to bring and return the employees from work and could perhaps be used for miscellaneous trips as might be required. Two stake-bed trucks will enter and leave the property once per day.

Other traffic is undeterminable at this time but would not create an excessive amount of traffic volume.

TRANSPORTATION OF MATERIALS:

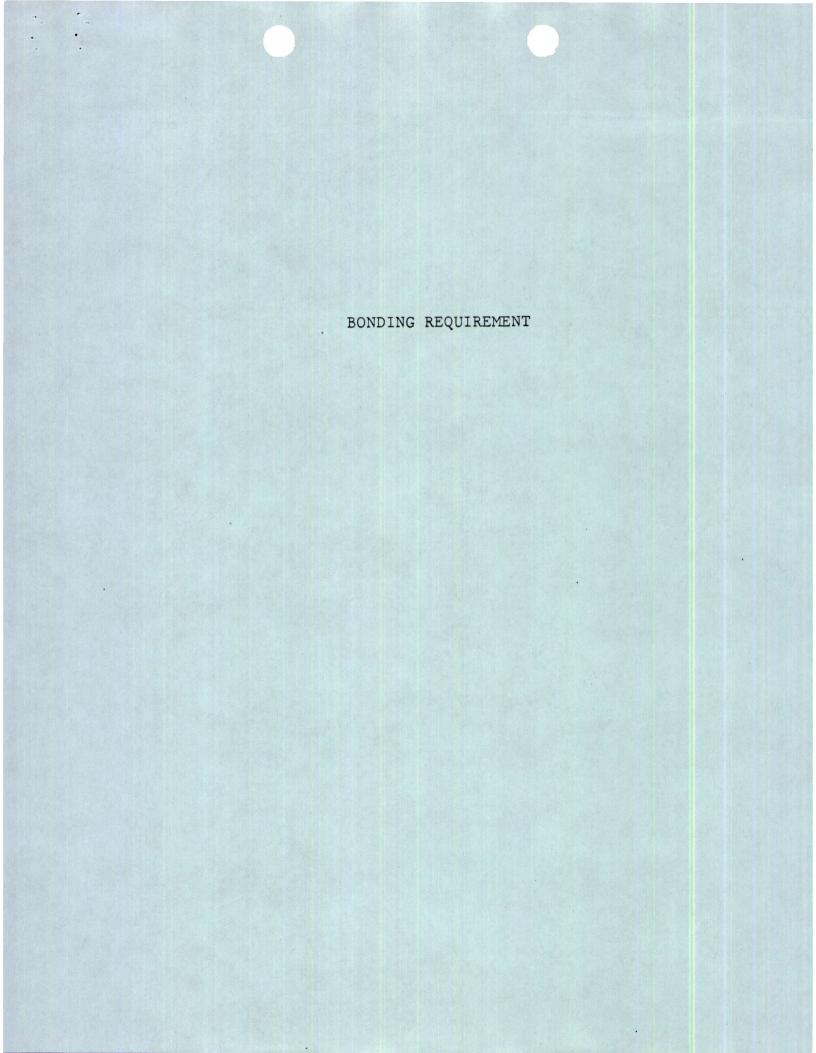
Concentrates will be transported from the mine site by two (2) stake-bed trucks carrying 55-gallon drums of material. It is anticipated that the trucks will make one to two trips per day.

STRUCTURES:

The only anticipated structure on the mine site will be the rest room facilities.

EQUIPMENT:

The maximum equipment anticipated will be two front-end loaders, two rock crushers, four spiral concentrators, two stake-bed trucks, a bull-dozer (as required only) and a dump truck (as required only).

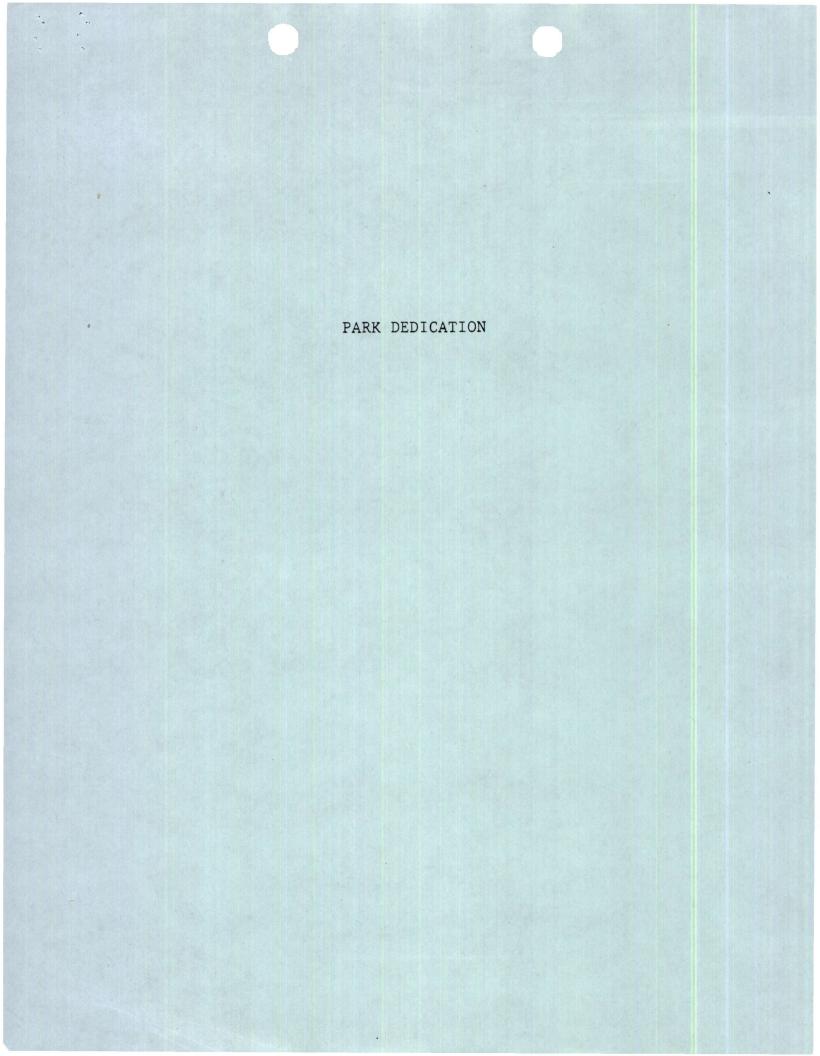


BONDING REQUIREMENTS

Both the BLM and the State Mining Division require posting a bond (one bond determined by which agency requires the greater amount) to insure proper reclamation. Before the final permit can be issued, this bond must be posted.

The State Mining Division has placed a bonding requirement of \$83,241.00. This bond will be met through a bonding agency, the Don F. Ensign Agency of Salt Lake City, Utah. Cost of the bond to Western International Corporation will be about one percent (1%) of the total amount.

The bond amount is somewhat negotiable. The State has indicated they would like to discuss it with us, so it is a possibility that it may be significantly lowered.



PARK DEDICATION

Immediately west of and adjacent to the Maple #2 Claim,
Park City Corporation owns five acres of land which they have
committed to a city park. Since it would be advantageous for
Park City to have a larger park, Western International Corporation
is willing to enter into an agreement with Park City Corporation.
to develop a park on the mining site and dedicate it to the
city upon the fulfillment of certain agreed upon conditions
and the completion of the mining activities.